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## FEATURES

- EXPANDED VALUE RANGE \& REDUCED CASE SIZES
- MOLDED CONSTRUCTION FOR HIGH SOLDERING HEAT RESISTANCE
- ELEVEN CASE SIZES (J, P, A2, A, B2, B, C2, C, V, D AND E)
- BOTH FLOW AND REFLOW SOLDERING APPLICABLE
- TAPE \& REEL PACKAGING COMPATIBLE WITH AUTOMATIC PICK \& PLACE EQUIPMENT

RoHS
Compliant
includes all homogeneous materials
*See Part Number System for Details
SPECIFICATIONS \& PERFORMANCE CHARACTERISTICS

| Capacitance Range | $0.1 \mu \mathrm{~F}$ to $680 \mu \mathrm{~F}$ |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Capacitance Tolerance | $\pm 20 \%$ (M), $\pm 10 \%$ (K) |  |  |  |  |  |  |  |  |
| Rated Voltage Range @ $85^{\circ} \mathrm{C}$ (Vdc) | 2.5 | 4.0 | 6.3 | 10 | 16 | 20 | 25 | 35 | 50 |
| Surge Voltage Rating @ $85^{\circ} \mathrm{C}$ (Vdc) | 3.3 | 5.2 | 8.0 | 13 | 20 | 28 | 33 | 46 | 85 |
| Derated Voltage @ $125^{\circ} \mathrm{C}$ (Vdc) | 1.8 | 2.5 | 4.0 | 6.3 | 10 | 13 | 16 | 22 | 32 |
| Operating Temperature Range | $-55^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ (to $+125^{\circ} \mathrm{C}$ with Derating) |  |  |  |  |  |  |  |  |
| Dissipation Factor | See Case Size and Specifications Table |  |  |  |  |  |  |  |  |
| Leakage Current @ $+25^{\circ} \mathrm{C}$ <br> (After 5 Minutes at Rated Voltage) | Not More Than 0.01 CV or $0.5 \mu \mathrm{~A}$, whichever is greater |  |  |  |  |  |  |  |  |
| Capacitance Change With Temperature | $-55^{\circ} \mathrm{C}$ |  |  | $+85^{\circ} \mathrm{C}$ |  |  | $+125^{\circ} \mathrm{C}$ |  |  |
| A2, A, B2, B, C, D \& E Case Size | $\Delta \mathrm{C}$ - 12\% |  |  | $\Delta C \pm 12 \%$ |  |  | $\Delta C \pm 12 \%$ |  |  |
| J \& P Case Size | $\Delta \mathrm{C}-20 \%$ |  |  | $\Delta \mathrm{C} \pm 20 \%$ |  |  | $\Delta \mathrm{C} \pm 20 \%$ |  |  |
| Resistance to Soldering Heat ( $+260^{\circ} \mathrm{C}$ for 5 Seconds) | $\Delta \mathrm{C} \pm 5 \%^{*} \mathrm{Max}, \mathrm{LC}=$ Less than initial specification. <br> DF = Less than initial specification |  |  |  |  |  |  |  |  |
| Moisture Resistance <br> (500 hours; 90~95\% RH @ 40º ) | $\Delta \mathrm{C} \pm 5 \%^{*}$ Max, LC $=$ Less than initial specification. <br> $D F=150 \%$ of initial specification |  |  |  |  |  |  |  |  |
| Temperature Cycling ( 5 cycles; $-55^{\circ} \mathrm{C} \sim+125^{\circ} \mathrm{C}$ ) | $\Delta \mathrm{C} \pm 5 \%^{*}$ Max, LC $=$ Less than initial specification. DF = Less than initial specification |  |  |  |  |  |  |  |  |
| Load Life (at Rated Voltage) (2,000 hours @ $85^{\circ} \mathrm{C}$ ) | $\Delta C \pm 10 \%{ }^{*}$ Max, $L C=125 \%$ of initial specification. <br> DF = Less than initial specification |  |  |  |  |  |  |  |  |
| Base Failure Rate (1.0 / Volt) | $1 \% / 1000$ hours at $60 \%$ confidence level ( $+85^{\circ} \mathrm{C}$ ) |  |  |  |  |  |  |  |  |

${ }^{*} \pm 12 \% \sim \pm 15 \%$ for extended values, $\pm 20 \%$ for J \& P case size values
POWER DISSIPATION @ $25^{\circ} \mathrm{C}$ (FREE AIR) \&
EQUIVALENT SERIES INDUCTANCE (ESL)
RIPPLE CURRENT CORRECTION FACTOR:

| Ambient Temperature | $25^{\circ} \mathrm{C}$ | $+55^{\circ} \mathrm{C}$ | $+85^{\circ} \mathrm{C}$ | $+105^{\circ} \mathrm{C}$ | $+125^{\circ} \mathrm{C}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Correction Factor | 1.0 | 0.90 | 0.80 | 0.40 | 0.15 |

## RIPPLE CURRENT/VOLTAGE RATINGS:

Imax. $=\sqrt{\frac{\mathrm{Pd}}{\mathrm{ESR}}} \quad V$ max. $=Z \bullet \sqrt{\frac{\mathrm{Pd}}{\mathrm{ESR}}}$
Imax. $=$ Ripple Current rating (Arms)
Pd = Power dissipation (watt)
ESR = Equivalent series resistance (ohm)
V max. $=$ Ripple voltage rating ( V rms)
$Z=$ The capacitors impedance $($ ohm $)=\sqrt{(E S R)^{2}+(X L-X C)^{2}}$

| Case <br> Code | Pd Max. <br> $(W)$ | ESL <br> $(\mathrm{nH})$ |
| :---: | :---: | :---: |
| P | 0.025 | 1.00 |
| A2 | 0.050 | 1.20 |
| A | 0.070 | 1.20 |
| B2 | 0.070 | 1.50 |
| B | 0.080 | 1.50 |
| C2 | 0.090 |  |
| C | 0.110 | 2.70 |
| V | 0.125 |  |
| D | 0.150 | 3.00 |
| E | 0.165 | 3.00 |

## PART NUMBER SYSTEM



Packaging: TR=Tape/Reel Voltage
Tolerance Code: $\mathrm{K}= \pm 10 \%, \mathrm{M}= \pm 20 \%$
Capacitance Code
Series

## STANDARD AND EXTENDED PRODUCT SPECIFICATIONS TABLE

*Extended Case Sizes
Chart show Case Size, Max. Tan $\delta$ @ $120 \mathrm{~Hz} /+20^{\circ} \mathrm{C}$, Max. ESR @ $100 \mathrm{KHz} /+20^{\circ} \mathrm{C}$

| $\begin{aligned} & \text { Cap } \\ & (\mu \mathrm{F}) \end{aligned}$ | Code | Working Voltage (Vdc) |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 2.5 | 4.0 | 6.3 | 10 | 16 | 20 | 25 | 35 | 50 |
| 0.1 | 104 | - | - | - | - | - | A2*6\%/40 | - | A 4\%/18 | - |
| 0.15 | 154 | - | - | - | - | - | A2*6\%/35 | - | A $4 \% / 18 \Omega$ | - |
| 0.22 | 224 | - | - | - | - | - | A2*6\%/35 | - | A $4 \% / 18 \Omega$ | B 4\%/14 |
| 0.33 | 334 | - | - | - | - | P 10\%/40 | A2*6\%/30 | - | A $4 \% / 15 \Omega$ | B 4\%/10 |
| 0.47 | 474 | - | - | - | - | P 10\%/35 | A2*6\%/27 | A $4 \% / 14 \Omega$ | $\begin{aligned} & \text { A* } 6 \% / 12 \Omega \\ & \text { B } 4 \% / 8.0 \Omega \end{aligned}$ | B 4\%/9.0 |
| 0.68 | 684 | - | - | - | P 10\%/25 | $\begin{aligned} & \hline \text { P } 10 \% / 25 \Omega \\ & \text { A2*6\%/25 } \end{aligned}$ | $\begin{gathered} \text { A2* } 6 \% / 15 \Omega \\ \text { A } 4 \% / 12 \Omega \\ \hline \end{gathered}$ | A*6\%/10 | $\begin{aligned} & \hline \text { A*6\%/9.0 } \\ & \text { B } 4 \% / 5.4 \Omega \end{aligned}$ | C 4\%/7.0 |
| 1.0 | 105 | - | - | P 10\%/25 | $\begin{aligned} & \text { P } 10 \% / 25 \Omega \\ & \text { A2* } 8 \% / 25 \Omega \end{aligned}$ | $\begin{gathered} \mathrm{J} 10 \% / 30 \Omega \\ \mathrm{P} 20 \% / 25 \Omega \\ \text { A1* } 6 \% / 16 \Omega \\ \text { A } 4 \% / 10 \Omega \end{gathered}$ | $\begin{gathered} \text { A2* } 6 \% / 13 \Omega \\ \text { A* } 6 \% / 9.0 \Omega \end{gathered}$ | $\begin{gathered} \mathrm{P} 6 \% / 8.0 \Omega \\ \mathrm{~A} 26 \% / 13 \Omega \\ \text { A*} 6 \% / 8.0 \Omega \end{gathered}$ | $\begin{gathered} \text { A2 } 6 \% / 13 \Omega \\ \text { A* } 6 \% / 8.0 \Omega \\ \text { B } 4 \% / 4.8 \Omega \end{gathered}$ | C 4\%/5.5 |
| 1.5 | 155 | - | P 10\%/25 | $\begin{aligned} & \text { P } 10 \% / 25 \Omega \\ & \text { A2* } 8 \% / 25 \Omega \end{aligned}$ | $\begin{gathered} \text { J } 20 \% / 30 \Omega \\ \text { P } 20 \% / 25 \Omega \\ \text { A2* } 8 \% / 20 \Omega \\ \text { A } 4 \% / 8.0 \Omega \end{gathered}$ | $\begin{gathered} \mathrm{J} 10 \% / 25 \Omega \\ \mathrm{~A} 2^{*} 6 \% / 13 \Omega \\ \mathrm{~A} 4 \% / 8.0 \Omega \end{gathered}$ | $\begin{gathered} \mathrm{A} 2 * 6 \% / 13 \Omega \\ \mathrm{~A} * 6 \% / 6.5 \Omega \end{gathered}$ | $\begin{gathered} \text { A*6\%/8.0 } \\ \text { B } 4 \% / 4.6 \Omega \end{gathered}$ | $\begin{aligned} & \mathrm{A}^{*} 6 \% / 8.0 \Omega \\ & \mathrm{~B} * 6 \% / 4.0 \Omega \\ & \mathrm{C} 4 \% / 3.0 \Omega \end{aligned}$ | C $4 \% / 4.0 \Omega$ |
| 2.2 | 225 | P 10\%/25 | $\begin{aligned} & \text { P } 10 \% / 25 \Omega \\ & \text { A2* } 8 \% / 25 \Omega \end{aligned}$ | J $20 \% / 20 \Omega$ P $20 \% / 20 \Omega$ A2* $8 \% / 18 \Omega$ A $4 \% / 8.0 \Omega$ | $\begin{gathered} \text { J } 20 \% / 30 \Omega \\ \text { P } 20 \% / 20 \Omega \\ \text { A2* } 8 \% / 12 \Omega \\ \text { A } 4 \% / 7.0 \Omega \\ \hline \end{gathered}$ | $\begin{gathered} \text { P } 10 \% / 19 \Omega \\ \text { A2*6\%/13 } \\ \text { A* } 6 \% / 6.0 \Omega \end{gathered}$ | $\begin{gathered} \hline \text { P } 10 \% / 8.0 \Omega \\ \text { A2 } 6 \% / 7.0 \Omega \\ \text { A* } 6 \% / 6.0 \Omega \\ \text { B } 4 \% / 3.5 \Omega \\ \hline \end{gathered}$ | $\begin{aligned} & \mathrm{A}^{*} 6 \% / 8.0 \Omega \\ & \mathrm{~B}^{\star} 6 \% / 4.0 \Omega \end{aligned}$ | $\begin{gathered} \mathrm{A} 6 \% / 5 \Omega \\ \mathrm{~B} * 6 \% / 4.2 \Omega \\ \mathrm{C} 4 \% / 3.0 \Omega \end{gathered}$ | D 4\%/1.8 |
| 3.3 | 335 | P 10\%/25 | $\begin{gathered} \text { P } 20 \% / 20 \Omega \\ \text { A2* } 8 \% / 18 \Omega \\ \text { A } 4 \% / 8.0 \Omega \end{gathered}$ | $\begin{gathered} \hline \text { J } 20 \% / 20 \Omega \\ \text { P } 20 \% / 13 \Omega \\ \text { A2* } 8 \% / 9.0 \Omega \\ \text { A } 4 \% / 7.5 \Omega \\ \hline \end{gathered}$ | $\begin{aligned} & \text { J } 20 \% / 25 \Omega \\ & \text { P } 20 \% / 20 \Omega \\ & \text { A2* } 8 \% / 12 \Omega \\ & \text { A* } 8 \% / 5.5 \Omega \end{aligned}$ | $\begin{gathered} \hline \text { P } 10 \% / 8.0 \Omega \\ \text { A2 } 8 \% / 7.0 \Omega \\ \text { A* } 6 \% / 5.0 \Omega \\ \text { B } 4 \% / 3.5 \Omega \end{gathered}$ | $\begin{gathered} \text { A2 } 8 \% / 5.0 \Omega \\ \text { A* } 6 \% / 5.0 \Omega \\ \text { B2 } 6 \% / 3.9 \Omega \\ \text { B*6\%/3.0 } \end{gathered}$ | A $6 \% / 7.0 \Omega$ B* $6 \% / 3.5 \Omega$ C $4 \% / 2.5 \Omega$ | $\begin{array}{\|c\|} \hline \text { B2 } 6 \% / 3.0 \Omega \\ \text { B*6\%/4.0 } \\ \text { C } 4 \% / 2.5 \Omega \\ \text { D } 4 \% / 2.0 \Omega \\ \hline \end{array}$ | D $4 \% / 1.4 \Omega$ |
| 4.7 | 475 | $\begin{aligned} & \text { P } 20 \% / 20 \Omega \\ & \text { A2* } 8 \% / 18 \Omega \end{aligned}$ | $\begin{gathered} \text { P } 20 \% / 12 \Omega \\ \text { A2* } 8 \% / 10 \Omega \\ \text { A } 4 \% / 7.5 \Omega \end{gathered}$ | $\begin{gathered} \text { J } 20 \% / 15 \Omega \\ \text { P } 20 \% / 12 \Omega \\ \text { A2* } 8 \% / 7.5 \Omega \\ \text { A* } 8 \% / 6.0 \Omega \end{gathered}$ | $\begin{gathered} \text { J } 20 \% / 10 \Omega \\ \text { P } 20 \% / 10 \Omega \\ \text { A2* } 8 \% / 8.0 \Omega \\ \text { A* } 8 \% / 5.0 \Omega \\ \text { B } 4 \% / 3.5 \Omega \end{gathered}$ | $\begin{gathered} \text { A2 } 8 \% / 4.5 \Omega \\ \text { A* } 6 \% / 5.0 \Omega \\ \text { B* } 6 \% / 3.0 \Omega \end{gathered}$ | $\begin{gathered} \hline \text { A2 } 15 \% / 5.0 \Omega \\ \text { A* } 6 \% / 5.0 \Omega \\ \text { B2 } 6 \% / 3.0 \Omega \\ \text { B }^{*} 6 \% / 3.0 \Omega \\ \text { C } 4 \% / 2.4 \Omega \\ \hline \end{gathered}$ | $\begin{gathered} \text { B2 } 6 \% / 3.0 \Omega \\ \text { B* } 6 \% / 3.0 \Omega \\ \text { C } 4 \% / 2.4 \Omega \end{gathered}$ | $\begin{aligned} & \text { C* } 6 \% / 2.2 \Omega \\ & \text { D } 4 \% / 1.5 \Omega \end{aligned}$ | D $4 \% / 1.4 \Omega$ |
| 6.8 | 685 | $\begin{aligned} & \text { P } 20 \% / 20 \Omega \\ & \text { A2* } 8 \% / 16 \Omega \end{aligned}$ | $\begin{gathered} \text { J } 20 \% / 15 \Omega \\ \text { P } 20 \% / 12 \Omega \\ \text { A2* } 8 \% / 8.0 \Omega \\ \text { A* } 8 \% / 6.0 \Omega \end{gathered}$ | $\begin{gathered} \text { J } 20 \% / 7.0 \Omega \\ \text { P } 20 \% / 12 \Omega \\ \text { A2* } 8 \% / 7.5 \Omega \\ \text { A }{ }^{*} 8 \% / 5.0 \Omega \\ \text { B } 6 \% / 3.5 \Omega \end{gathered}$ | $\begin{gathered} \mathrm{A} 28 \% / 8.0 \Omega \\ \text { A } 8 \% / 4.5 \Omega \\ \mathrm{~B} 8 \% / 3.0 \Omega \end{gathered}$ | $\begin{gathered} \text { A2* } 2 \% / 5.0 \Omega \\ \text { A }^{*} 6 \% / 5.0 \Omega \\ \text { B2 } 6 \% / 5.0 \Omega \\ \text { B* } 6 \% / 2.5 \Omega \\ \text { C } 6 \% / 1.9 \Omega \end{gathered}$ | $\begin{gathered} \mathrm{B} 26 \% / 3.0 \Omega \\ \mathrm{~B} * 6 \% / 2.8 \Omega \\ \mathrm{C} 6 \% / 1.9 \Omega \end{gathered}$ | B $6 \% / 2.5 \Omega$ C* $6 \% / 1.9 \Omega$ D $6 \% / 1.4 \Omega$ | $\begin{aligned} & C * 6 \% / 1.9 \Omega \\ & 0 \% / 1.30 \end{aligned}$ | - |
| 10 | 106 | $\begin{aligned} & \text { J } 20 \% / 12 \Omega \\ & \text { P } 20 \% / 12 \Omega \\ & \text { A2* } 8 \% / 15 \Omega \end{aligned}$ | $\begin{gathered} \text { J } 20 \% / 12 \Omega \\ \text { P } 20 \% / 12 \Omega \\ \text { A2 } 2.12 \% / 8.0 \Omega \\ \text { A* } 8 \% / 5.0 \Omega \\ \text { B } 6 \% / 3.5 \Omega \end{gathered}$ | $\begin{gathered} \text { J } 20 \% / 8.0 \Omega \\ \text { P } 20 \% / 12 \Omega \\ \text { A2* } 8 \% / 10 \Omega \\ \text { A* } 8 \% / 4.0 \Omega \\ \text { B } 6 \% / 3.0 \Omega \end{gathered}$ | $\begin{gathered} \hline \mathrm{P} 20 \% / 6.0 \Omega \\ \mathrm{~A} 28 \% / 5.0 \Omega \\ \mathrm{~A} * 8 \% / 3.2 \Omega \\ \mathrm{~B} 2 * 8 \% / 3.2 \Omega \\ \mathrm{~B} * 8 \% / 2.5 \Omega \\ \mathrm{C} 6 \% / 1.8 \Omega \\ \hline \end{gathered}$ | $\begin{gathered} \text { A } 8 \% / 5.0 \Omega \\ \text { B2 } 8 \% / 4.0 \Omega \\ \text { B* } 6 \% / 2.4 \Omega \\ \text { C } 6 \% / 1.8 \Omega \end{gathered}$ | $\begin{aligned} & \mathrm{B}^{*} 6 \% / 2.5 \Omega \\ & \text { C* } 6 \% / 1.8 \Omega \\ & \text { D } 6 \% / 1.3 \Omega \end{aligned}$ | $\begin{gathered} \mathrm{C} 26 \% / 2.0 \Omega \\ \mathrm{C} * 6 \% / 1.8 \Omega \\ \mathrm{D} 6 \% / 1.2 \Omega \end{gathered}$ | $\begin{aligned} & \mathrm{C} 6 \% / 1.5 \Omega \\ & \mathrm{D} 6 \% / 1.0 \Omega \\ & \mathrm{E} * 6 \% / 1.0 \Omega \end{aligned}$ | - |
| 15 | 156 | $\begin{gathered} \mathrm{J} 20 \% / 8.0 \Omega \\ \text { A2*12\%/10 } \\ \text { A* } 8 \% / 5.0 \Omega \end{gathered}$ | $\begin{gathered} \mathrm{P} 20 \% / \\ \mathrm{A} 2^{*} 12 \% / 8.0 \Omega \\ \mathrm{~A}^{*} 8 \% / 4.0 \Omega \\ \mathrm{~B}^{*} 8 \% / 3.0 \Omega \end{gathered}$ | P $20 \% / 5.0 \Omega$ A2 $12 \% / 4.0 \Omega$ A ${ }^{*} 8 \% / 3.5 \Omega$ B2 $8 \% / 3.5 \Omega$ B* $8 \% / 2.5 \Omega$ C $6 \% / 1.8 \Omega$ | $\begin{gathered} \text { A2 } 20 \% / 3.0 \Omega \\ \text { B2* } 8 \% / 2.5 \Omega \\ \text { C } 6 \% / 1.8 \Omega \end{gathered}$ | $\begin{gathered} \text { A } 12 \% / 5.0 \Omega \\ \text { B2* } 6 \% / 2.5 \Omega \\ \text { C* } 6 \% / 1.8 \Omega \\ \text { D } 6 \% / 1.8 \Omega \end{gathered}$ | $\begin{aligned} & \text { C*6\%/1.7 } \\ & \text { D } 6 \% / 0.8 \Omega \end{aligned}$ | $\begin{aligned} & \mathrm{C} 6 \% / 1.5 \Omega \\ & \mathrm{D} * 6 \% / 1.0 \Omega \end{aligned}$ | D*6\%0.9 | - |
| 22 | 226 | $\begin{gathered} \text { P } 20 \% / 4.0 \Omega \\ \text { A2*12\%/10 } \\ \text { A* } 8 \% / 4.0 \Omega \end{gathered}$ | P $20 \% / 5.0 \Omega$ A2 $12 \% / 4.0 \Omega$ A* $8 \% / 3.5 \Omega$ B2 $8 \% / 3.5 \Omega$ B* $8 \% / 2.8 \Omega$ C $6 \% / 1.8 \Omega$ | $\begin{array}{\|c\|} \hline \text { P } 20 \% / 4.0 \Omega \\ \text { A2 } 12 \% / 2.8 \Omega \\ \text { A }^{*} 10 \% / 4.5 \Omega \\ B^{*} 12 \% / 4.5 \Omega \\ \text { B* } 8 \% / 2.3 \Omega \\ \text { C } 6 \% / 1.8 \Omega \\ \hline \end{array}$ | A $12 \% / 2.5 \Omega$ B2 $12 \% / 4.0 \Omega$ $B^{*} 8 \% / 2.4 \Omega$ $C^{*} 8 \% / 1.8 \Omega$ D $6 \% / 1.5 \Omega$ | $\begin{array}{\|c} \text { B2 } 10 \% / 2.2 \Omega \\ \text { B*6\%/2.5 } \\ \text { C*6\%/1.6 } \\ \text { D } 6 \% / 0.8 \Omega \end{array}$ | $\begin{gathered} \mathrm{C} 26 \% / 1.4 \Omega \\ \mathrm{C} * 6 \% / 1.5 \Omega \\ \mathrm{D} * 6 \% / 0.8 \Omega \end{gathered}$ | D*6\%/0.8 | - | - |
| 33 | 336 | $\begin{gathered} \text { P } 20 \% / 5.0 \Omega \\ \text { A2 } 12 \% / 4.0 \Omega \\ \text { A } 8 \% / 3.5 \Omega \\ \text { B2*8\%/3.5 } \\ \text { B* } 8 \% / 3.0 \Omega \end{gathered}$ | $\begin{gathered} \hline \mathrm{P} 20 \% / 4.0 \Omega \\ \mathrm{~A} 28 \% / 4.5 \Omega \\ \mathrm{~A}^{*} 10 \% / 4.5 \Omega \\ \mathrm{~B} 212 \% / 4.5 \Omega \\ \mathrm{~B} \text { * } 8 \% / 2.4 \Omega \\ \mathrm{C} 6 \% / 1.8 \Omega \\ \hline \end{gathered}$ | A2 $18 \% / 3.0 \Omega$ <br> A $12 \% / 5.0 \Omega$ B2 12\%/1.7 $\Omega$ B*8\%/2.0 $\Omega$ C*8\%/1.8 $\Omega$ D $6 \% / 1.5 \Omega$ | $\begin{array}{\|c} \text { B2 } 12 \% / 1.7 \Omega \\ \text { B}^{\star} 8 \% / 2.0 \Omega \\ \text { C* } 8 \% / 1.6 \Omega \\ \text { D } 6 \% / 0.8 \Omega \end{array}$ | $\begin{gathered} \mathrm{B} 8 \% / 1.4 \Omega \\ \mathrm{C} 26 \% / 1.4 \Omega \\ \text { C* } 6 \% / 1.2 \Omega \\ \text { D*6\%/0.8 } \end{gathered}$ | D*6\%/0.8 | D 6\%/0.7 | - | - |

## Highlighting Denotes New Values

NIC COMPONENTS CORP. www.niccomp.com I www.lowESR.com I www.RFpassives.com I www.SMTmagnetics.com

## STANDARD AND EXTENDED PRODUCT SPECIFICATIONS TABLE

*Extended Case Sizes
Chart Shows Case Sizes, Max. Tan $\delta @ 120 \mathrm{~Hz} / 20^{\circ} \mathrm{C}$, Max. ESR @ $100 \mathrm{KHz} / 20^{\circ} \mathrm{C}$

| $\begin{aligned} & \text { Cap } \\ & (\mu \mathrm{F}) \\ & \hline \end{aligned}$ | Code | Working Voltage (Vdc) |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 2.5 | 4.0 | 6.3 | 10 | 16 | 20 | 25 |
| 47 | 476 | P 30\%/6.0 <br> A2 12\%/4.5 $\Omega$ <br> A*12\%/4.5 $\Omega$ <br> B2*12\%/4.5 $\Omega$ <br> B* $8 \% / 2.4 \Omega$ | P 30\%/3.0 <br> A2 $15 \% / 4.5 \Omega$ <br> A $12 \% / 5.0 \Omega$ <br> B2 12\%/3.0 B* $8 \% / 2.0 \Omega$ C*8\%/1.8 $\Omega$ D $6 \% / 1.2 \Omega$ | A $12 \% / 2.0 \Omega$ <br> B2 12\%/3.0 $\Omega$ <br> B* $8 \% / 2.0 \Omega$ <br> C*8\%/1.6 <br> D 6\%/0.8 | $\begin{gathered} \mathrm{B} 8 \% / 3.0 \Omega \\ \mathrm{C} 28 \% / 1.0 \Omega \\ \mathrm{C} * 8 \% / 1.6 \Omega \\ \mathrm{D} * 8 \% / 0.8 \Omega \end{gathered}$ | $\begin{aligned} & \text { C*6\%/1.2 } \\ & \text { D*6\%/0.8 } \end{aligned}$ | D*6\%0.8 $\Omega$ |  |
| 68 | 686 | $\begin{gathered} \text { A } 18 \% / 3.0 \Omega \\ \mathrm{~B}^{\star} 8 \% / 2.0 \Omega \end{gathered}$ | A $12 \% / 2.5 \Omega$ <br> B2 15\%/3.0 <br> B* $8 \% / 2.0 \Omega$ <br> C* $8 \% / 1.6 \Omega$ <br> D $6 \% / 0.8 \Omega$ | A $30 \% / 2.0 \Omega$ B2 $20 \% / 2.0 \Omega$ B $10 \% / 1.8 \Omega$ C2 $10 \% / 0.8 \Omega$ C* $8 \% 1.2 \Omega$ D* $8 \% / 0.8 \Omega$ | $\left\lvert\, \begin{array}{\|c\|} \hline \text { B } 12 \% / 0.9 \Omega \\ \text { C2 } 10 \% / 1.0 \Omega \\ C^{*} 8 \% / 1.2 \Omega \\ D^{*} 8 \% / 0.8 \Omega \end{array}\right.$ | $\begin{aligned} & \mathrm{C} 6 \% / 0.7 \Omega \\ & \mathrm{D} * 6 \% / 0.7 \Omega \end{aligned}$ | - |  |
| 100 | 107 | $\begin{array}{\|c\|} \hline \text { A } 30 \% / 2.0 \Omega \\ \text { B2 18\%/2.0 } \\ \text { B*8\%/2.0 } \end{array}$ | A 30\%/2.0 B2 20\%/1.3 $\Omega$ B*12\%/2.0 $\Omega$ C2 10\%/0.8 $\Omega$ C* $8 \% / 1.2 \Omega$ D*8\%/0.8 $\Omega$ | $\begin{gathered} \text { B2 } 20 \% / 1.3 \Omega \\ \text { B } 12 \% / 1.2 \Omega \\ \text { C2 } 10 \% / 0.8 \Omega \\ \text { C}^{*} 0 \% / 0.9 \Omega \\ \text { D}^{*} 8 \% / 0.8 \Omega \end{gathered}$ | $\left\lvert\, \begin{array}{\|c\|} \hline \mathrm{C} 210 \% / 0.8 \Omega \\ \mathrm{C} 10 \% / 1.2 \Omega \\ \mathrm{~V} 8 \% / 0.5 \Omega \\ \mathrm{D} * 8 \% / 0.7 \Omega \end{array}\right.$ | D*10\%/1.0 $\Omega$ | - | - |
| 150 | 157 | A $30 \% / 2.0 \Omega$ <br> B2 $20 \% / 1.0 \Omega$ <br> B*16\%/5.0 <br> C2 $12 \% / 0.8 \Omega$ <br> B2 | $\begin{array}{\|c\|} \hline \mathrm{B} 18 \% / 2.0 \Omega \\ \mathrm{C} 210 \% / 0.8 \Omega \\ \mathrm{C}^{*} 10 \% / 1.0 \Omega \\ \mathrm{D}^{*} 8 \% / 0.7 \Omega \\ \hline \end{array}$ | $\begin{aligned} & \text { B } 12 \% / 1.0 \Omega \\ & \text { C } 10 \% / 1.2 \Omega \\ & \text { D } 8 \% / 0.7 \Omega \end{aligned}$ | $\begin{gathered} V 8 \% / 0.5 \Omega \\ D^{*} 10 \% / 0.7 \Omega \end{gathered}$ | D*6\%/0.9 ${ }^{\text {a }}$ | - | - |
| 220 | 227 | B2 $30 \% / 1.0 \Omega$ B $18 \% / 20 \Omega$ C2 $12 \% / 0.8 \Omega$ $C^{*} 12 \% / 1.0 \Omega$ | $\begin{aligned} & \text { B } 18 \% / 0.5 \Omega \\ & \text { C } 12 \% / 1.2 \Omega \\ & \text { D}^{*} 8 \% / 0.7 \Omega \end{aligned}$ | $\begin{aligned} & \text { C } 14 \% / 1.2 \Omega \\ & \text { V } 12 \% / 0.5 \Omega \\ & \text { D*12\%/0.8 } \end{aligned}$ | $\begin{gathered} \text { D } 12 \% / 1.0 \Omega \\ E^{*} 8 \% / 0.9 \Omega \end{gathered}$ | - | - | - |
| 330 | 337 | $\begin{aligned} & \text { B } 25 \% / 0.6 \Omega \\ & \text { C } 16 \% / 1.2 \Omega \end{aligned}$ | $\begin{aligned} & \hline \mathrm{C} 14 \% / 1.2 \Omega \\ & \text { V } 12 \% / 0.5 \Omega \\ & \mathrm{D} * 14 \% / 0.7 \Omega \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { V } 14 \% / 0.5 \Omega \\ & \text { D } 14 \% / 1.0 \Omega \end{aligned}$ | - | - | - | - |
| 470 | 477 | $\begin{aligned} & \hline \mathrm{B} 35 \% / 0.6 \Omega \\ & \mathrm{C} 18 \% / 1.2 \Omega \\ & \mathrm{D} * 14 \% / 0.7 \Omega \end{aligned}$ | D 16\%/1.0 | D 20\%/0.3 | - | - | - | - |
| 680 | 687 |  | D 24*/0.3 | - | - | - | - | - |

Highlighting Denotes New Values
DIMENSIONS (mm)

| Case Code | Metric Code | English Code | L | W | H | P | a |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| J | 1608 | 0603 | $1.6 \pm 0.1$ | $0.8 \pm 0.1$ | $0.8 \pm 0.1$ | $0.3 \pm 0.15$ | $0.6 \pm 0.1$ |
| P | 2012 | 0805 | $2.0 \pm 0.2$ | $1.25 \pm 0.2$ | 1.2 MAX. | $0.5 \pm 0.2$ | $0.9 \pm 0.1$ |
| A2 | 3216 | 1206 | $3.2 \pm 0.2$ | $1.6 \pm 0.2$ | 1.2 MAX. | $0.8 \pm 0.3$ | $1.2 \pm 0.1$ |
| A | 3216 | 1206 | $3.2 \pm 0.2$ | $1.6 \pm 0.2$ | $1.6 \pm 0.2$ | $0.8 \pm 0.3$ | $1.2 \pm 0.1$ |
| B2 | 3528 | 1411 | $3.5 \pm 0.2$ | $2.8 \pm 0.2$ | 1.2 MAX. | $0.8 \pm 0.3$ | $2.3 \pm 0.1$ |
| B | 3528 | 1411 | $3.5 \pm 0.2$ | $2.8 \pm 0.2$ | $1.9 \pm 0.2$ | $0.8 \pm 0.3$ | $2.2 \pm 0.1$ |
| C2 | 6032 | 2412 | $6.0 \pm 0.3$ | $3.2 \pm 0.3$ | 1.5 MAX. | $1.3 \pm 0.3$ | $2.2 \pm 0.1$ |
| C | 6032 | 2412 | $6.0 \pm 0.3$ | $3.2 \pm 0.3$ | $2.6 \pm 0.3$ | $1.3 \pm 0.3$ | $2.2 \pm 0.1$ |
| V | 7343 | 2916 | $7.3 \pm 0.2$ | $4.3 \pm 0.2$ | 2.0 MAX. | $1.3 \pm 0.3$ | $2.4 \pm 0.1$ |
| D | 7343 | 2916 | $7.3 \pm 0.2$ | $4.3 \pm 0.2$ | $2.9 \pm 0.3$ | $1.3 \pm 0.3$ | $2.4 \pm 0.1$ |
| E | 7343 H | 2917 | $7.3 \pm 0.2$ | $4.3 \pm 0.2$ | $4.1 \pm 0.2$ | $1.3 \pm 0.3$ | $2.4 \pm 0.1$ |

J, P, A, A2, C, V, D \& E CASE SIZE


B \& B2 CASE SIZE


Terminations:
100\% Sn (Lead-Free)
Standard

CAPACITANCE CODES

| Cap. ( $\mu \mathrm{F}$ ) | $\begin{aligned} & \text { STD } \\ & \text { EIA Code } \end{aligned}$ | $\begin{aligned} & \text { EIA Code } \\ & \text { 198D } \end{aligned}$ | $\begin{gathered} \text { Code for } \\ \text { P Case Size } \end{gathered}$ | Code for J Case Size |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | 2.5Vdc | 4Vdc | 6.3 Vdc | 10 Vdc | 16 Vdc |
| 0.1 | 104 | A5 | - | - | - | - | - | C |
| 0.15 | 154 | E5 | - | - | - | - | - | - |
| 0.22 | 224 | J5 | - | - | - | - | - | - |
| 0.33 | 334 | N5 | N | - | - | - | - | - |
| 0.47 | 474 | S5 | S | - | - | - | - | - |
| 0.68 | 684 | W5 | W | - | - | - | - | - |
| 1.0 | 105 | A6 | A | - | - | - | - | - |
| 1.5 | 155 | E6 | E | - | - | - | A | - |
| 2.2 | 225 | J6 | J | - | - | $\Gamma$ | < | - |
| 3.3 | 335 | N6 | N | - | - | $\bigcirc$ | - | - |
| 4.7 | 475 | S6 | S | - | - | J | D | - |
| 6.8 | 685 | W6 | W | - | G | c | - | - |
| 10 | 106 | A7 | $\overline{\mathrm{A}}$ | e | (1) | $\bar{\Gamma}$ | - | - |
| 22 | 226 | J7 | J | - |  | - | - | - |
| 33 | 336 | N7 | $\bar{N}$ | - | - | - | - | - |
| 47 | 476 | S7 | $\overline{\mathrm{S}}$ | - | - | - | - | - |

## PRODUCTION CODE

| Year | Month |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sept | Oct | Nov | Dec |
| 2005 | A | B | C | D | E | F | G | H | J | K | L | M |
| 2006 | N | P | Q | R | S | T | U | V | W | X | Y | Z |
| 2007 | a | b | C | d | e | f | g | h | j | k | I | m |
| 2008 | n | p | q | r | S | t | u | V | w | X | y | z |



VOLTAGE CODES

| Vottage | Code |
| :---: | :---: |
| 2.5 | e |
| 4 | G |
| 6.3 | J |
| 10 | A |
| 16 | C |
| 20 | D |
| 25 | E |
| 35 | V |
| 50 | H |

COMPONENT MARKING
J Case Size


C, V \& D Case Size
2.5 V marked $2,6.3 \mathrm{~V}$ marked 6


RECOMMENDED LAND
PATTERN DIMENSIONS (mm)

| Case Size | a | b | c |
| :---: | :---: | :---: | :---: |
| J | 0.90 | 0.70 | 1.00 |
| P | 1.05 | 0.50 | 1.20 |
| A \& A2 | 1.35 | 1.10 | 1.50 |
| B \& B2 | 1.35 | 1.40 | 2.70 |
| C | 2.00 | 2.90 | 2.70 |
| D | 2.05 | 4.10 | 2.90 |
| D | 2.05 | 4.10 | 2.90 |



TAPE DIMENSIONS (mm)

| Metric Code | Case Code | $\mathrm{A}_{0} \pm 0.2$ | $\mathrm{B}_{0} \pm 0.2$ | $W \pm 0.3$ | $F \pm 0.05$ | $\mathrm{P}_{0} \pm 0.1$ | $\mathrm{P}_{0} \pm 0.1$ | $\mathrm{P}_{0} \pm 0.05$ | $\mathrm{G} \pm 0.1$ | $\mathrm{K} \pm 0.2$ | T | 7" Reel |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1608 | J | 1.0 | 1.8 | 8.0 | 3.5 | 4.0 | 2.0 | 2.0 | 1.75 | 1.1 | 0.2 | 4000 |
| 2012 | P | 1.4 | 2.2 | 8.0 | 3.5 | 4.0 | 4.0 | 2.0 | 1.75 | 1.4 | 0.2 | 3000 |
| 3216 | A2 | 1.0 | 3.5 | 8.0 | 3.5 | 4.0 | 4.0 | 2.0 | 1.75 | 1.4 | 0.2 | 3000 |
| 3216 | A | 1.9 | 3.5 | 8.0 | 3.5 | 4.0 | 4.0 | 2.0 | 1.75 | 1.9 | 0.2 | 2000 |
| 3528 | B2 | 3.2 | 3.8 | 8.0 | 3.5 | 4.0 | 4.0 | 2.0 | 1.75 | 1.4 | 0.2 | 3000 |
| 3528 | B | 3.2 | 3.8 | 8.0 | 3.5 | 4.0 | 4.0 | 2.0 | 1.75 | 2.1 | 0.2 | 2000 |
| 6032 | C | 3.7 | 6.4 | 12.0 | 5.65 | 4.0 | 8.0 | 2.0 | 1.5 | 3.0 | 0.3 | 500 |
| 7343 | D | 4.8 | 7.7 | 12.0 | 5.65 | 4.0 | 8.0 | 2.0 | 1.5 | 3.3 | 0.3 | 500 |
| 7343H | E | 4.7 | 7.7 | 12.0 | 5.5 | 4.0 | 8.0 | 2.0 | 1.5 | 4.5 | 0.6 | 500 |



## REEL DIMENSIONS (mm)

| Tape <br> Width | A | C | D | E | N | $\mathrm{W}_{1}$ | $\mathrm{~W}_{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 8 mm | $178 \pm 2.0$ | $13 \pm 0.5$ | $21 \pm 0.5$ | $2.0 \pm 0.5$ | 50 min. | $10 \pm 2.0$ | 14.5 max. |
| 12 mm | $178 \pm 2.0$ | $13 \pm 0.5$ | $21 \pm 0.5$ | $2.0 \pm 0.5$ | 50 min. | $14.5 \pm 2.0$ | 18.5 max. |



Cover tape peel-off specification

1. Peel-off speed : $300 \mathrm{~mm} / \mathrm{min}$.
2. Peel-off force : $\mathrm{F}=30-75 \mathrm{~g}$
3. Peel-off angle : $\quad \Theta=0-15^{\circ}$

Peel-off speed $(F)=50 \mathrm{~mm} / \mathrm{Sec}$.


NIC COMPONENTS CORP. www.niccomp.com I www.lowESR.com I www.RFpassives.com I www.SMTmagnetics.com

